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## **Magnetohydrodynamic Fluid Flow Past Contracting Surface in a Rotating System**

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### **Abstract**

Heat and mass transfer past a contracting surface in a rotating system has been discussed. In this study, the governing equations are transformed into a system of partial differential equations and solved numerically using finite difference method. The solutions are presented graphically for various parameters. The results obtained are applicable in areas such as polymer technology, metallurgy, cooling of metallic plates; control of boundary layer along a liquid film in condensation processes, cooling of micro electromechanical systems, shrink packaging, cooling of nuclear reactor.

**Keywords:** Rotation; radiation; contracting surfaces; MHD.

### **1. Introduction**

Fluid is defined as a substance that deforms continuously when acted on by a shearing stress of any magnitude. Fluids can be characterized as Newtonian and non-Newtonian fluids. For Newtonian fluids the shearing stress is linearly related to the rate of shearing strain but for non-Newtonian fluids shearing stress is not linearly related to the rate of shearing strain. Water, air, mercury, kerosene and thin lubricating oils are Newtonian fluids whereas paints, coal tar, blood and grease represent for non-Newtonian fluids.

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Magnetohydrodynamics (MHD) is the science of the motion of electrically conducting fluids in presence of magnetic fields. MHD studies the dynamics of the interaction of electrically conducting fluids and the electromagnetic field. The fluids can be ionized gases (commonly known as plasma) or liquid metals. The flow of an electrically conducting fluid under a magnetic field in general gives rise to induced electric currents. The induced currents flow in the direction perpendicular to both the magnetic field and the direction of the motion of the fluid. The importance of studying fluid dynamics is the analysis of systems involving fluid flow, heat transfer and associated phenomena such as diffusion, convection, dissipation, boundary layers and turbulence by means of computer based simulation. All of these phenomena are governed by the compressible Navier-Stokes equations.

Some of applications of the boundary layer flow include wire drawing, paper production, glass-fiber production, liquid metal, polymer sheet synthesis, continuous stretching of plastic films and artificial fibers etc. In all these cases, the mechanical properties of the final product are appreciably affected by the rate of cooling and stretching in the process and material characteristics could therefore be manipulated to desired specifications [1]. Flow due to a shrinking sheet is different from the stretching sheet flow. A stretching sheet regime induces far field suction towards the sheet, while a shrinking sheet intensifies the velocity away from the sheet. Shrinking sheet flows are important in the manufacture of certain polymers and high-performance materials for aerospace coatings [2].

Most researchers have studied wide variety of flow situations. Some of these studies can be found in work of [3] studied flow and heat transfer of a fluid through a porous medium over a stretching surface with internal heat generation/ absorption and suction/ blowing. [4] Studied thermal diffusion and chemical reaction effects on unsteady MHD free convection flow past a semi infinite vertical permeable moving plate. [5] investigated numerical steady free convection flow through a porous medium around a rectangular isothermal body. [6] studied free convective mass transfer flow past infinite vertical porous plate with Soret effect.

Following are some research on effects of radiation, heat generation and viscous dissipation [7] presented work on MHD free convection heat and mass transfers of a heat generations fluid past an impulsively started infinite porous plate with Hall currents and radiation absorption. [8] Studied combined effects of thermal radiation and hall current on MHD free-convective flow and mass transfer over a stretching sheet with Variable Viscosity. The study of MHD rotating system had considerable progress in the last few decades. For instance [9] studied MHD Flow in Porous Media over A Stretching Surface in Rotating System with Hall Currents, Heat and Mass Transfer.

Also researchers have analyzed problems of flow over shrinking surface under various conditions. [10] Studied effects of thermal radiation on MHD viscous fluid flow and heat transfer over non linear shrinking porous sheet. Reference [11] Studied combined effects of variable magnetic field and porous medium on the flow of MHD fluid due to exponentially shrinking sheet.

Less emphasis has been given to the problems of flow due to a contracting sheet. The aim of this work is therefore to investigate MHD stokes fluid flow problem and combined effects of various parameters on velocity,

temperature and concentration past a porous contracting surface in a rotating system.

## 2. Mathematical formulation

Consider flow of an incompressible, electrically conducting, and viscous Newtonian fluid past a contracting electrically non-conducting sheet embedded in porous media in a rotating system.

A second impermeable and electrically non conducting sheet is placed parallel to the contracting sheet for closed flow. The system is rotated with constant angular velocity  $\Omega$ , the y axis is taken to be infinite. The surface of the contracting sheet is maintained at a uniform temperature  $T_w$ . The free stream temperature and concentration of species are  $T_\infty$  and  $C_\infty$  respectively. An upward flow is established along the surface when  $T_w > T_\infty$  due to free convection; and there is a down flow when  $T_\infty > T_w$

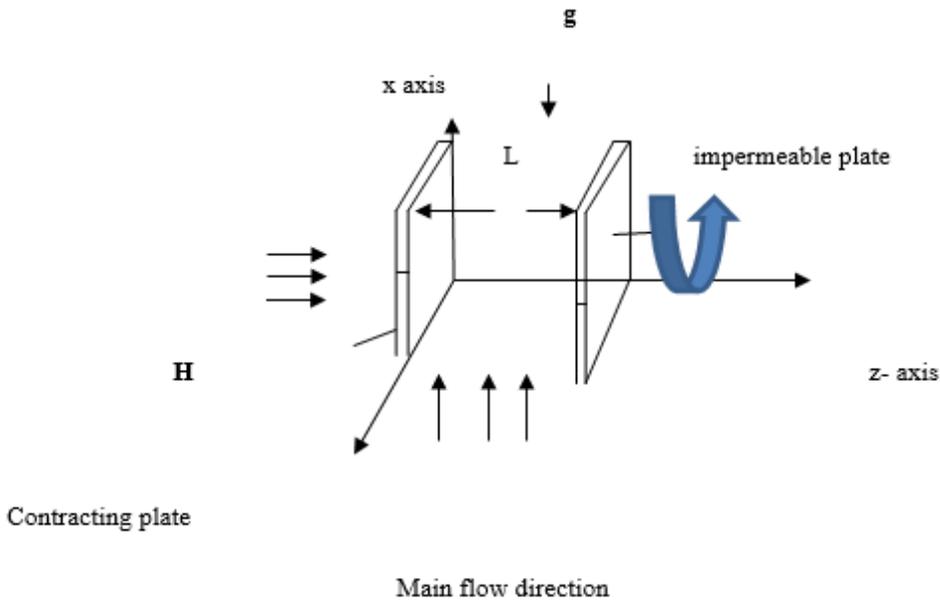


Figure 1.0: Flow configuration

The governing equations governing the flow are as follow:

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + \omega_0 \frac{\partial u}{\partial z} - 2\Omega v = v \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial z^2} \right) - u \frac{v}{k_p} + \frac{\sigma \mu^2 B^2 u}{\rho} + \beta g (T - T_\infty) + \beta^* g (C - C_\infty) \quad (1)$$

$$\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + \omega_0 \frac{\partial v}{\partial z} + 2\Omega v = v \left( \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial z^2} \right) - v \frac{v}{k_p} - \frac{\sigma \mu^2 B^2 v}{\rho} \quad (2)$$

$$\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + \omega_0 \frac{\partial T}{\partial z} = \frac{k_f}{\rho c_p} \left( \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial z^2} \right) + \frac{D_m k_T}{c_s c_p} \left( \frac{\partial^2 C}{\partial x^2} + \frac{\partial^2 C}{\partial z^2} \right) \frac{\mu}{\rho c_p} \left[ \left( \frac{\partial u}{\partial z} \right)^2 + \left( \frac{\partial v}{\partial z} \right)^2 \right] + \frac{\sigma \mu^2 B^2 (u^2 + v^2)}{\rho c_p} - \frac{16 \sigma^* T_\infty^3}{3 \rho c_p k^*} \frac{\partial^2 T}{\partial z^2}$$
(3)

$$\frac{\partial C}{\partial t} + u \frac{\partial C}{\partial x} - \omega_0 \frac{\partial C}{\partial z} = D_m \left( \frac{\partial^2 C}{\partial x^2} + \frac{\partial^2 C}{\partial z^2} \right) + \frac{D_m k_T}{T} \left( \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial z^2} \right) - u \frac{\partial C}{\partial x} + \omega_0 \frac{\partial C}{\partial z}$$
(4)

The initial and boundary conditions of this problem are:

$$t \leq 0 : u = 0, v = 0, \omega = 0, T = 0, H = 0, C = 0 \text{ at } 0 \leq z \leq L$$

$$t > 0 : u = u_\infty, v = 0, T = T_\infty, C = C_\infty, H = H_0, \text{ at } x = 0 \text{ Channel entrance}$$

$$t > 0 : u = -cx^n, v = 0, T = T_w, C = C_w, H = H_0 x^{\frac{n-1}{2}}, \text{ at } z = 0 \text{ (porous wall)}$$
(5)

$$t > 0 : u = 0, v = 0, T = T_w, C = C_w, H = H_0, \text{ at } z = L \text{ (impermeable wall)}$$

### Non-Dimensionalisation

Non-dimensionalization is aimed at ensuring that the results are applicable to other geometrically similar configurations under a similar set of flow conditions. The characteristic length is taken as perpendicular distance  $L$  units between the parallel sheets. The characteristic velocity is taken as the free stream velocity  $U_\infty$ .

The non-dimensional Variables are defined as follow;

$$u' = \frac{u}{U_\infty}, v' = \frac{v}{U_\infty}, \omega' = \frac{\omega_0}{U_\infty}, t' = \frac{U_\infty t}{L}, z' = \frac{z}{L}, T' = \frac{T - T_\infty}{T_w - T_\infty}$$
(6)

Governing equations in non dimensional form:

$$\frac{\partial u'}{\partial t'} + u' \frac{\partial u'}{\partial x'} - \omega' \frac{\partial u'}{\partial z'} - Rov' = \frac{1}{\text{Re}} \left( \frac{\partial^2 u'}{\partial x'^2} + \frac{\partial^2 u'}{\partial z'^2} \right) - Xiu' - Mu' + Gr_\theta T' + Gr_c C'$$
(7)

$$\frac{\partial v'}{\partial t'} + u' \frac{\partial v'}{\partial x'} - \omega' \frac{\partial v'}{\partial z'} + Rou' = \frac{1}{\text{Re}} \left( \frac{\partial^2 v'}{\partial x'^2} + \frac{\partial^2 v'}{\partial z'^2} \right) - Xiv' - Mv''$$
(8)

$$\frac{\partial T'}{\partial t'} + u' \frac{\partial T'}{\partial x'} - \omega_0 \frac{\partial T'}{\partial z'} = \frac{1}{\text{Re}} \left[ \frac{1}{\text{Pr}} \left( \frac{\partial^2 T'}{\partial x'^2} + \frac{\partial^2 T'}{\partial z'^2} \right) \right] + D_f \text{Re} \left( \frac{\partial^2 C'}{\partial x'^2} + \frac{\partial^2 C'}{\partial z'^2} \right) + \frac{Ec}{\text{Re}} \left[ \left( \frac{\partial u'}{\partial z'} \right)^2 + \left( \frac{\partial v'}{\partial z'} \right)^2 \right] - \frac{4}{3N \text{Pr Re}} \left( \frac{\partial^2 T'}{\partial z'^2} \right) + R \text{Re} (u'^2 + v'^2) \tag{9}$$

$$\frac{\partial C'}{\partial t'} + u' \frac{\partial C'}{\partial x'} - \omega \frac{\partial C'}{\partial z'} = \frac{1}{\text{Re Sc}} \left( \frac{\partial^2 C'}{\partial x'^2} + \frac{\partial^2 C'}{\partial z'^2} \right) + \frac{Sr}{\text{Re}} \left( \frac{\partial^2 T'}{\partial x'^2} + \frac{\partial^2 T'}{\partial z'^2} \right) \tag{10}$$

Where  $M = \frac{\sigma \mu_e^2 H^2}{\rho U_\infty}$  is the magnetic field parameter,  $\text{Re} = \frac{U_\infty L}{\nu}$  is the Reynolds number,  $Xi = \frac{g L}{U_\infty k_p}$  is

the permeability parameter,  $Gr_\theta = \frac{\beta g L (T_w - T_\infty)}{U_\infty^2}$  is the local temperature Grashof number,  $Ro = \frac{2\Omega}{U_\infty^2}$  is

rotational parameter, Where  $\text{Pr} = \frac{\mu c_p}{k_f}$  is prandlt number,  $N = \frac{k^* k_f}{4\sigma^* T_\infty^3}$  is the radiation parameter,

$D_f = \frac{\rho D_m k_f (C_w - C_\infty)}{\mu c_s c_p (T_w - T_\infty)}$  is Dufour number,  $Ec = \frac{U^2}{c_p \Delta T}$  is the Eckert number,  $R = \frac{\sigma \mu_e^2 H^2}{\rho^2 c_p \Delta T}$  is the

Joule heating parameter and  $\Delta T$  represents the temperature differences.  $(T_w - T_\infty)$ .

Where  $Sc = \frac{\mu}{\rho D_m}$  is the schimidt number,  $Sr = \frac{\rho D_m k_f (T_w - T_\infty)}{\mu T_m (C_w - C_\infty)}$  is the soret number

The initial and boundary conditions in non-dimensional form:

$$t' < 0 : u' = 0, v' = 0, T' = 0, C' = 0, H' = 0, at, z = 0 \text{ at } 0 \leq z \leq L$$

$$t' > 0 : u' = 1, v' = 0, T' = 1, C' = 1, H' = 1, at, z = 0 \text{ Channel entrance}$$

$$t' > 0 : u' = \frac{-c L x^n}{U_\infty}, v' = 0, T' = 1, C' = 1, H' = x^{\frac{n-1}{2}}, at, z = 0 \text{ (porous wall)} \tag{11}$$

$$t' > 0 : u' = 0, v' = 0, T' =, C' = 1, H' = 1, at, z = L \text{ (Impermeable wall)}$$

### 3. Methodology

Equations that govern MHD flow past contracting surface in a rotating system with heat and mass transfer

transfers are non-linear. The equations are solved using finite differences method that applies Crank-Nicholson algorithm. The finite difference method replaces each PDE with a discrete approximation for space and time domain. Governing equations in finite difference form.

$$\begin{aligned} & \frac{U_{i,j}^{k+1} - U_{i,j}^k}{\Delta t} + U_{i,j}^k \left( \frac{U_{i,j}^{k+1} - U_{i-1,j}^k + U_{i,j}^k - U_{i-1,j}^k}{2\Delta x} \right) - w_0 \left( \frac{U_{i,j}^{k+1} - U_{i-1,j}^k + U_{i,j}^k - U_{i-1,j}^k}{2\Delta z} \right) - \frac{R_0}{2} (V_{i,j}^{k+1} + V_{i,j}^k) \\ &= \frac{1}{2(\Delta x)^2 \text{Re}} (U_{i+1,j}^{k+1} - 2U_{i,j}^{k+1} + U_{i-1,j}^{k+1} + U_{i+1,j}^k - 2U_{i,j}^k + U_{i-1,j}^k) + \frac{1}{2(\Delta z)^2 \text{Re}} (U_{i+1,j}^{k+1} - 2U_{i,j}^{k+1} + U_{i-1,j}^{k+1} + U_{i+1,j}^k - 2U_{i,j}^k + U_{i-1,j}^k) \\ & - \frac{Xi}{2} (U_{i,j}^{k+1} + U_{i,j}^k) - \frac{M}{2} (U_{i,j}^{k+1} + U_{i,j}^k) + \frac{Gr_\theta}{2} (T_{i,j}^{k+1} + T_{i,j}^k) + \frac{Gr_c}{2} (C_{i,j}^{k+1} + C_{i,j}^k) \end{aligned} \tag{12}$$

$$\begin{aligned} & \frac{V_{i,j}^{k+1} - V_{i,j}^k}{\Delta t} + U_{i,j}^k \left( \frac{V_{i,j}^{k+1} - V_{i-1,j}^k + V_{i,j}^k - V_{i-1,j}^k}{2\Delta x} \right) - w_0 \left( \frac{V_{i,j}^{k+1} - V_{i-1,j}^k + V_{i,j}^k - V_{i-1,j}^k}{2\Delta z} \right) \\ & + \frac{R_0}{2} (U_{i,j}^{k+1} + U_{i,j}^k) = \frac{1}{2(\Delta x)^2 \text{Re}} (V_{i+1,j}^{k+1} - 2V_{i,j}^{k+1} + V_{i-1,j}^{k+1} + V_{i+1,j}^k - 2V_{i,j}^k + V_{i-1,j}^k) \\ & + \frac{1}{2(\Delta z)^2 \text{Re}} (V_{i+1,j}^{k+1} - 2V_{i,j}^{k+1} + V_{i-1,j}^{k+1} + V_{i+1,j}^k - 2V_{i,j}^k + V_{i-1,j}^k) - \frac{Xi}{2} (V_{i,j}^{k+1} + V_{i,j}^k) - \frac{M}{2} (V_{i,j}^{k+1} + V_{i,j}^k) \end{aligned} \tag{13}$$

$$\begin{aligned} V_{i,j}^{k+1} &= V_{i,j}^k + \frac{\Delta t}{2(\Delta x)^2 \text{Re}} (V_{i+1,j}^{k+1} + V_{i-1,j}^{k+1} + V_{i+1,j}^k - 2V_{i,j}^k + V_{i-1,j}^k) + \frac{\Delta t}{2(\Delta z)^2 \text{Re}} (V_{i+1,j}^{k+1} + V_{i-1,j}^{k+1} + V_{i+1,j}^k - 2V_{i,j}^k + V_{i-1,j}^k) \\ & + \frac{\Delta t}{2\Delta x} U_{i,j}^k (V_{i-1,j}^{k+1} - V_{i,j}^k + V_{i-1,j}^k) + \frac{\Delta t w_0}{2\Delta z} (V_{i-1,j}^{k+1} - V_{i,j}^k + V_{i-1,j}^k) - \frac{\Delta t Xi}{2} V_{i,j}^k - \frac{\Delta t M}{2} V_{i,j}^k \\ & + \frac{\Delta t R_0}{2} (U_{i,j}^{k+1} + U_{i,j}^k) / (1 + \frac{\Delta t}{2\Delta x} V_{i,j}^k - \frac{w_0 \Delta t}{2\Delta z} + \frac{\Delta t}{\text{Re}(\Delta z)^2} + \frac{\Delta t}{\text{Re}(\Delta x)^2} + \frac{\Delta t Xi}{2} + \frac{\Delta t M}{2}) \end{aligned} \tag{14}$$

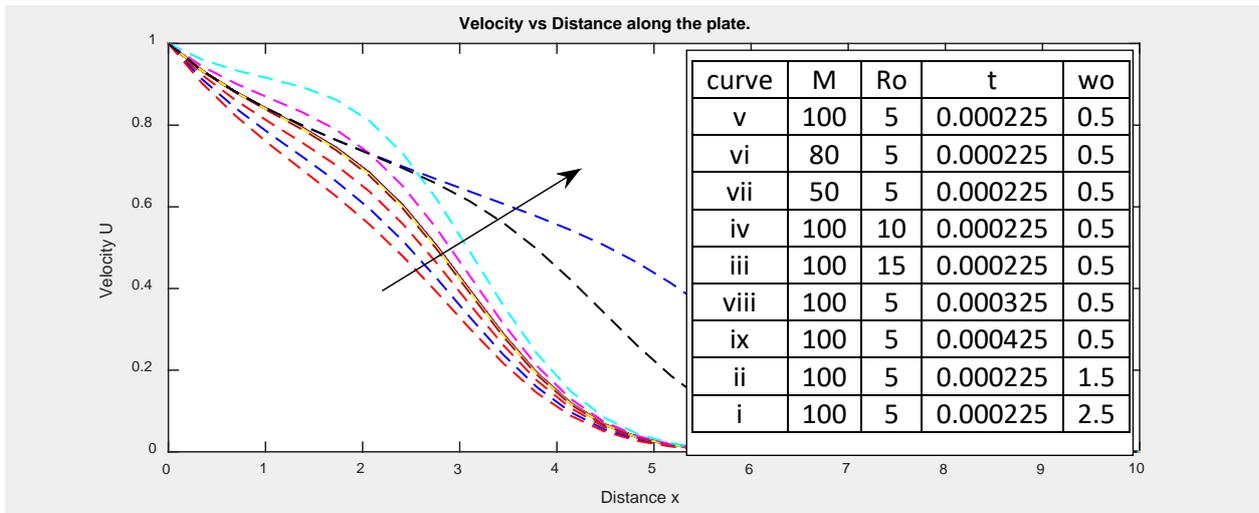
$$\begin{aligned} & \frac{T_{i,j}^{k+1} - T_{i,j}^k}{\Delta t} + U_{i,j}^k \left( \frac{T_{i,j}^{k+1} - T_{i-1,j}^k + T_{i,j}^k - T_{i-1,j}^k}{2\Delta x} \right) - w_0 \left( \frac{T_{i,j}^{k+1} - T_{i-1,j}^k + T_{i,j}^k - T_{i-1,j}^k}{2\Delta z} \right) \\ &= \frac{1}{2(\Delta x)^2 \text{Pr Re}} (T_{i+1,j}^{k+1} - 2T_{i,j}^{k+1} + T_{i-1,j}^{k+1} + T_{i+1,j}^k - 2T_{i,j}^k + T_{i-1,j}^k) \\ & + \frac{1}{2(\Delta z)^2 \text{Pr Re}} (T_{i+1,j}^{k+1} - 2T_{i,j}^{k+1} + T_{i-1,j}^{k+1} + T_{i+1,j}^k - 2T_{i,j}^k + T_{i-1,j}^k) + \frac{Ec}{\text{Re}} \left[ \left( \frac{U_{i,j}^{k+1} - U_{i-1,j}^{k+1} + U_{i,j}^k - U_{i-1,j}^k}{2\Delta x} \right)^2 + \left( \frac{V_{i,j}^{k+1} - V_{i-1,j}^{k+1} + V_{i,j}^k - V_{i-1,j}^k}{2\Delta z} \right)^2 \right] \\ & - \frac{2}{3Ni \text{Pr Re} (\Delta z)^2} (T_{i+1,j}^{k+1} - 2T_{i,j}^{k+1} + T_{i-1,j}^{k+1} + T_{i+1,j}^k - 2T_{i,j}^k + T_{i-1,j}^k) + R \text{Re} \left[ \left( \frac{U_{i,j}^{k+1} + U_{i,j}^k}{2} \right)^2 + \left( \frac{V_{i,j}^{k+1} + V_{i,j}^k}{2} \right)^2 \right] \\ & + D_f \text{Re} \left( \frac{C_{i+1,j}^{k+1} - 2C_{i,j}^{k+1} + C_{i-1,j}^{k+1} + C_{i+1,j}^k - 2C_{i,j}^k + C_{i-1,j}^k}{2(\Delta x)^2} \right) + D_f \text{Re} \left( \frac{C_{i+1,j}^{k+1} - 2C_{i,j}^{k+1} + C_{i-1,j}^{k+1} + C_{i+1,j}^k - 2C_{i,j}^k + C_{i-1,j}^k}{2(\Delta z)^2} \right) \end{aligned}$$

(15)

$$\begin{aligned} & \frac{C_{i,j}^{k+1} - C_{i,j}^k}{\Delta t} + U_{i,j}^k \left( \frac{C_{i,j}^{k+1} - C_{i-1,j}^k + C_{i,j}^k - C_{i-1,j}^k}{2\Delta x} \right) - w_0 \left( \frac{C_{i,j}^{k+1} - C_{i-1,j}^k + C_{i,j}^k - C_{i-1,j}^k}{2\Delta z} \right) \\ &= \frac{1}{2(\Delta x)^2 Sc Re} (C_{i+1,j}^{k+1} - 2C_{i,j}^{k+1} + C_{i-1,j}^{k+1} + C_{i+1,j}^k - 2C_{i,j}^k + C_{i-1,j}^k) \\ &+ \frac{1}{2(\Delta z)^2 Sc Re} (C_{i+1,j}^{k+1} - 2C_{i,j}^{k+1} + C_{i-1,j}^{k+1} + C_{i+1,j}^k - 2C_{i,j}^k + C_{i-1,j}^k) \\ &+ \frac{Sr}{Re} \left[ \left( \frac{T_{i+1,j}^{k+1} - 2T_{i,j}^{k+1} + T_{i-1,j}^{k+1} + T_{i+1,j}^k - 2T_{i,j}^k + T_{i-1,j}^k}{2(\Delta x)^2} \right) + \left( \frac{T_{i+1,j}^{k+1} - 2T_{i,j}^{k+1} + T_{i-1,j}^{k+1} + T_{i+1,j}^k - 2T_{i,j}^k + T_{i-1,j}^k}{2(\Delta z)^2} \right) \right] \end{aligned} \tag{16}$$

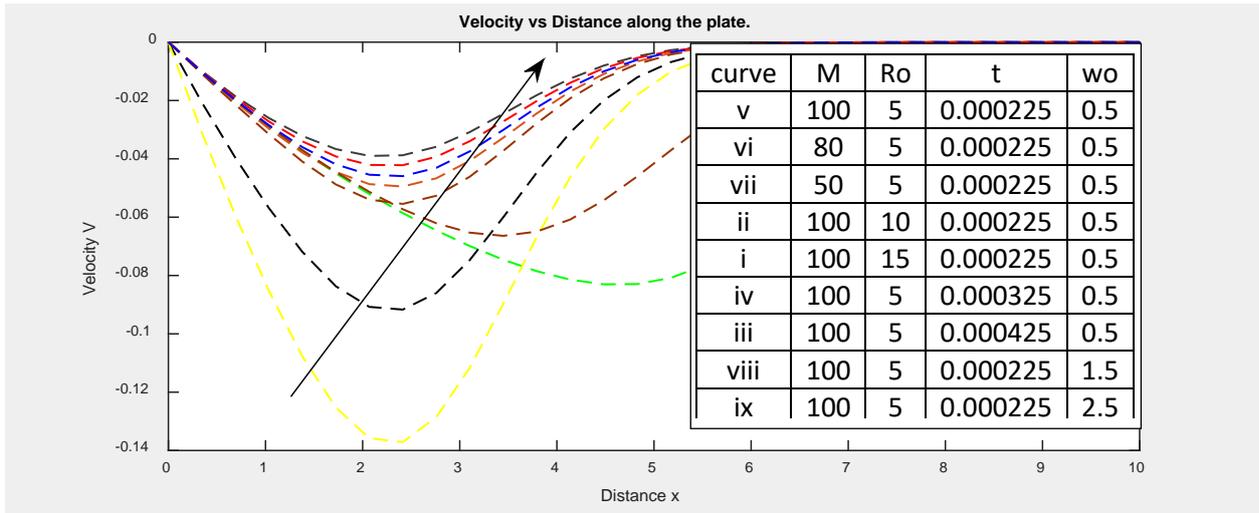
**4. Discussion of the results**

Various parameters that have been varied include the Reynold’s number Re, Rotational parameter Ro, Permeability parameter Xi, local mass Grashof number , time t, Dufour number Df, Nusselt number Nu, Eckert number Ec, Soret number Sr, Schmidt number Sc, and suction parameter .

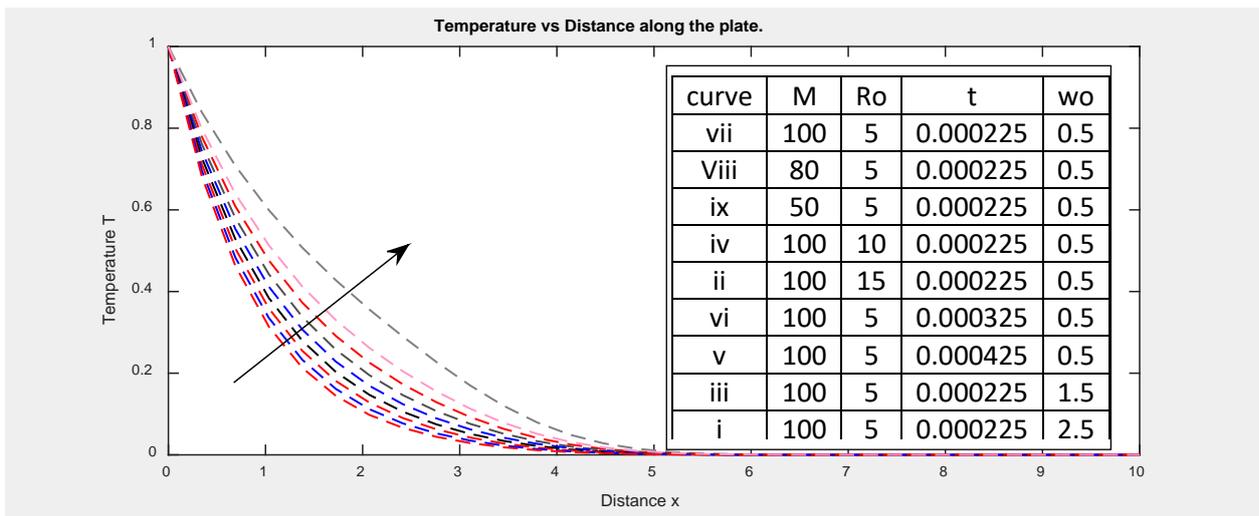


**Figure 2.0:** Primary velocity profiles for different values of Magnetic parameter M, rotation parameter, time and suction parameter  $W_0$ , for Grashof number  $Gr_\theta = -0.5$

From figure 2 and 3 it is noted that increase in Magnetic parameter lead to a decrease in both primary and secondary velocity profiles. An increase in rotation parameter lead to a decrease in primary velocity profiles and an increase in secondary velocity profiles. Increase in time causes an increase in primary and secondary velocity. Increase in suction parameter causes a decrease in primary velocity profile and secondary velocity profiles.

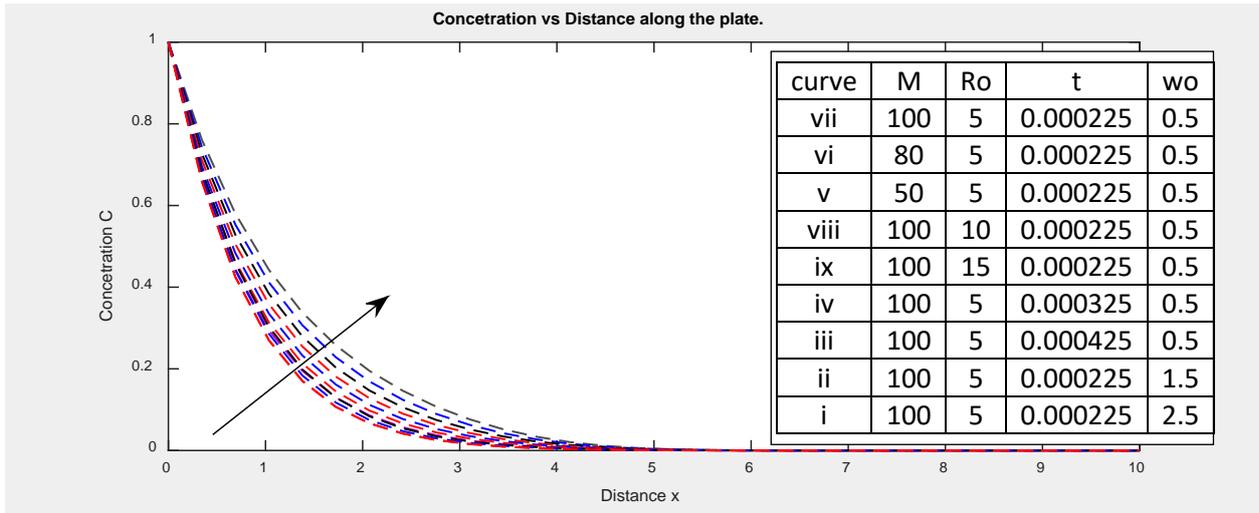


**Figure 3:** Secondary velocity profiles for different values of Magnetic parameter M, rotation parameter, time and suction parameter  $W_0$ , for Grashof number  $Gr_\theta = -0.5$ .



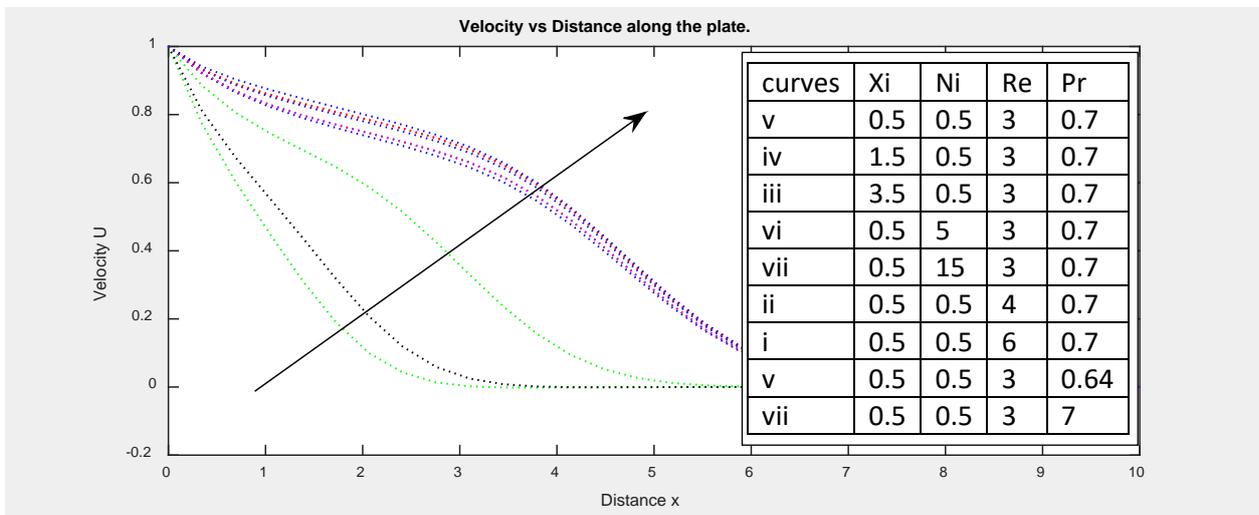
**Figure 4:** Temperature profiles for different values of Magnetic parameter M, rotation parameter, time and suction parameter  $W_0$ , for Grashof number  $Gr_\theta = -0.5$ .

From figure 4 it is noted that increase in M causes a decrease in the temperature profiles. The temperature profiles decrease with increasing M. The reduced velocity by the frictional drag due to the Lorentz force is responsible for reducing thermal viscous dissipation in the fluid leading to a thinner thermal boundary layer. An increase in Ro causes a decrease in the temperature profiles. An increase in time decreases the temperature. An increase in the magnitude of the suction parameter causes a decrease in the temperature profiles.



**Figure 5:** Concentration profiles for different values of Magnetic parameter  $M$ , rotation parameter, time and suction parameter  $W_0$ , for Grashof number  $Gr_\theta = -0.5$ .

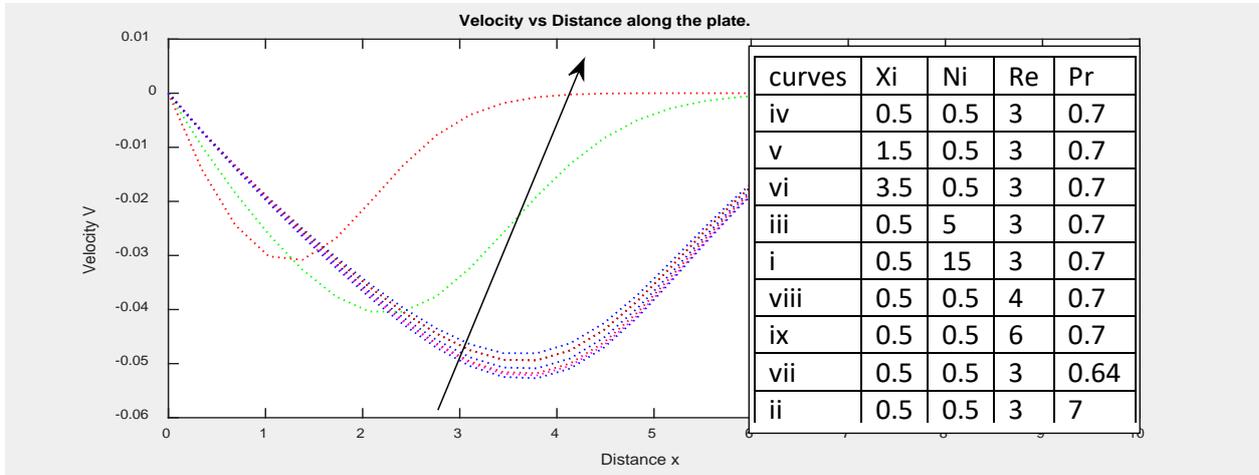
From figure 5 it is noted that an increase in  $M$  causes an increase in the concentration profiles. An increase in  $Ro$  causes an increase in the concentration profiles. An increase in time decreases the concentration profiles. An increase in the magnitude of the suction parameter causes a decrease in the concentration profiles.



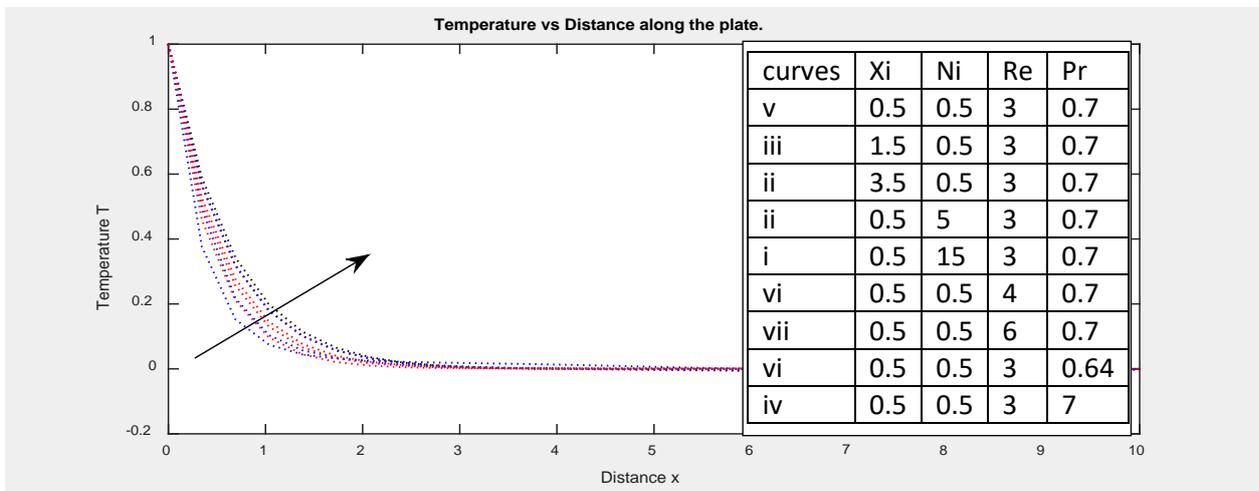
**Figure 6:** Primary velocity profiles for different values of permeability parameter  $X_i$ , radiation parameter  $N$ , Reynolds number  $Re$ , Prandtl number  $Pr$  for  $Gr_\theta = -0.5$ .

From Figure 6 and 7 it is noted that an increase in permeability  $X_i$  causes a decrease in the primary velocity and secondary velocity profiles respectively. The permeability parameter  $X_i$  is inversely proportional to the actual permeability  $k_p$  of the porous medium. Increase in  $X_i$  leads to deceleration of the flow hence the velocity decreases. Increasing  $X_i$ , increases the resistance of the porous medium (as the permeability physically becomes less with increasing  $X_i$ ). This decelerates the flow and reduces the magnitudes of both the primary and

secondary velocity respectively. An increase in radiation parameter  $N$  leads to increase in primary velocity profiles and secondary velocity profiles respectively. Increase in Reynolds' number  $Re$  causes a decrease in the primary and secondary velocity profiles and then to an increase due to cross over. The Reynolds's number represents the ratio of the inertial to viscosity forces.



**Figure 7:** Secondary velocity profiles for different values of permeability parameter  $X_i$ , radiation parameter  $N$ , Reynolds number  $Re$ , Prandtl number  $Pr$  for  $Gr_\theta = -0.5$

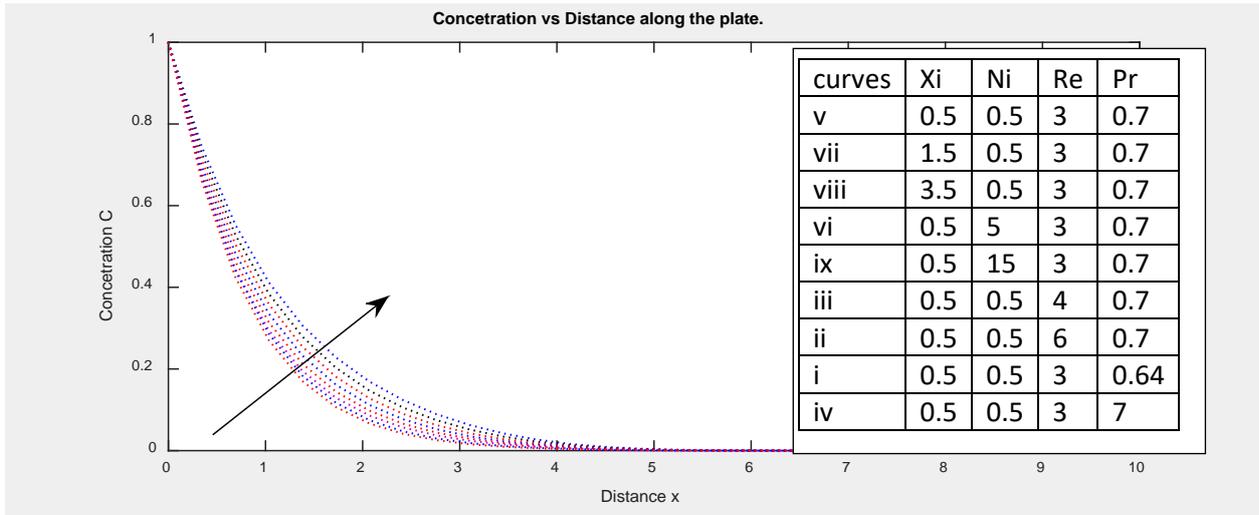


**Figure 8:** Temperature profiles for different values of permeability parameter  $X_i$ , radiation parameter  $N$ , Reynolds number  $Re$ , Prandtl number  $Pr$  for  $Gr_\theta = -0.5$

Increase in  $Re$  results to a large inertial force that in turn translates to a higher velocity. An increase in Prandtl number causes an increase of both primary and secondary velocity profiles. It's higher in water as compared to air and gases.

From figure 8 it is noted that an increase in permeability  $X_i$  causes a decrease in the temperature profiles. An increase in  $N$  leads to a decrease in the temperature profiles. An increase in Reynolds's number causes increase

in temperature profiles. An increase in Prandtl number causes a decrease in temperature profiles.



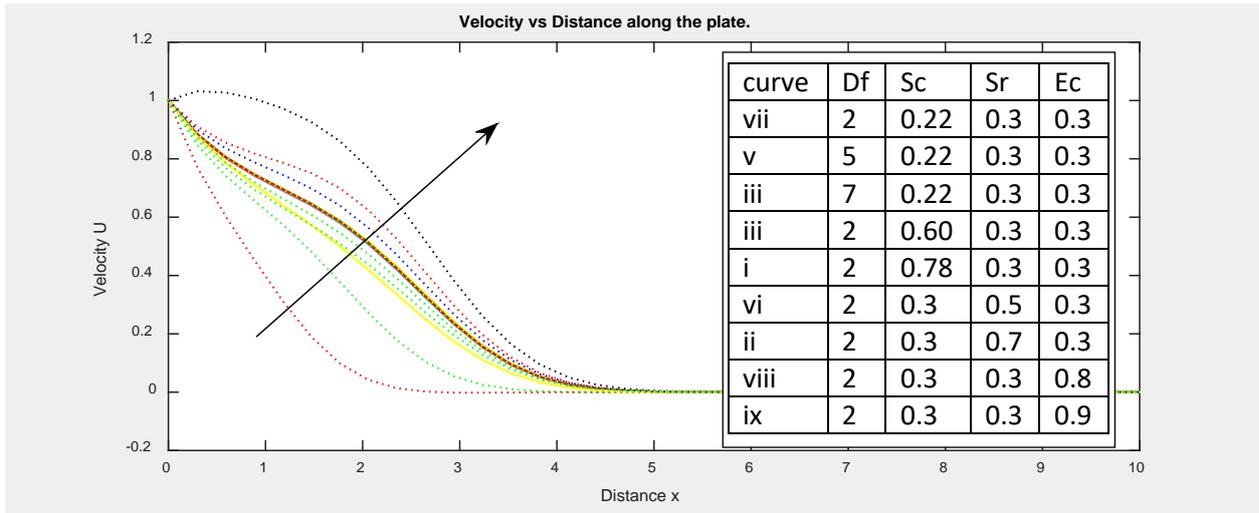
**Figure 9:** Concentration profiles for different values of permeability parameter  $X_i$ , radiation parameter  $N$ , Reynolds number  $Re$ , Prandtl number  $Pr$  for  $Gr_\theta = -0.5$

From figure 9 it is noted that an increase in  $X_i$  reduces the rate of species transportation from the surface of the contracting sheet, leading to an increase in the concentration profiles. An increase in  $N$  leads to an increase in the concentration profiles.

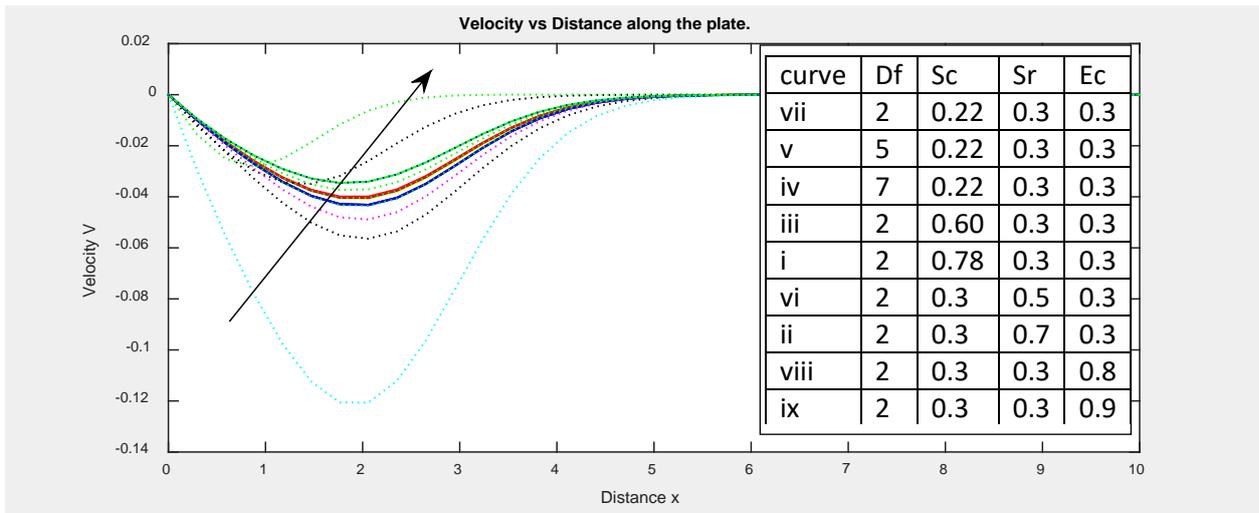
An increase in  $Re$  causes a decrease in the concentration profiles. A higher velocity of the fluid takes away more species from the surface of the contracting sheet thereby reducing the species concentration. Increase in Prandtl number causes a decrease in concentration profiles. From figure 10 and 11 it is noted that an increase in the Dufour number  $Df$  causes decrease in the primary and secondary velocity profiles. An increase in Schmidt number  $Sc$  causes a decrease in primary profiles and secondary velocity profiles. A large value of  $Sc$  means a presence of a heavier fluid and this implies a lower velocity of the fluid. An increase in  $Sr$  causes a decrease in the primary and secondary velocity profiles. An increase in Eckert number  $Ec$  causes an increase in the primary and secondary velocity profiles. The Eckert number expresses the relationship between the kinetic energy in the flow and the enthalpy. It embodies the conversion of kinetic energy into internal energy by work done against the viscous fluid stresses. A positive Eckert number implies cooling the sheet, implying heating the fluid. This causes a rise in the velocity of the fluid respectively.

From figure 12 it is noted that an increase in  $Df$  causes a decrease in the temperature profiles. The Dufour number signifies the contribution of the concentration gradients to the thermal energy flux in the flow. From the definition of the Dufour number, an increase in  $Df$  translates directly to a decrease in the temperature profiles of the fluid, or to an increase in the concentration profiles of the fluid. An increase in  $Sc$  leads to a decrease in the temperature profiles. An increase in  $Sr$  causes a decrease in the temperature profiles.

An increase in Eckert number  $Ec$  causes an increase in the temperature profiles

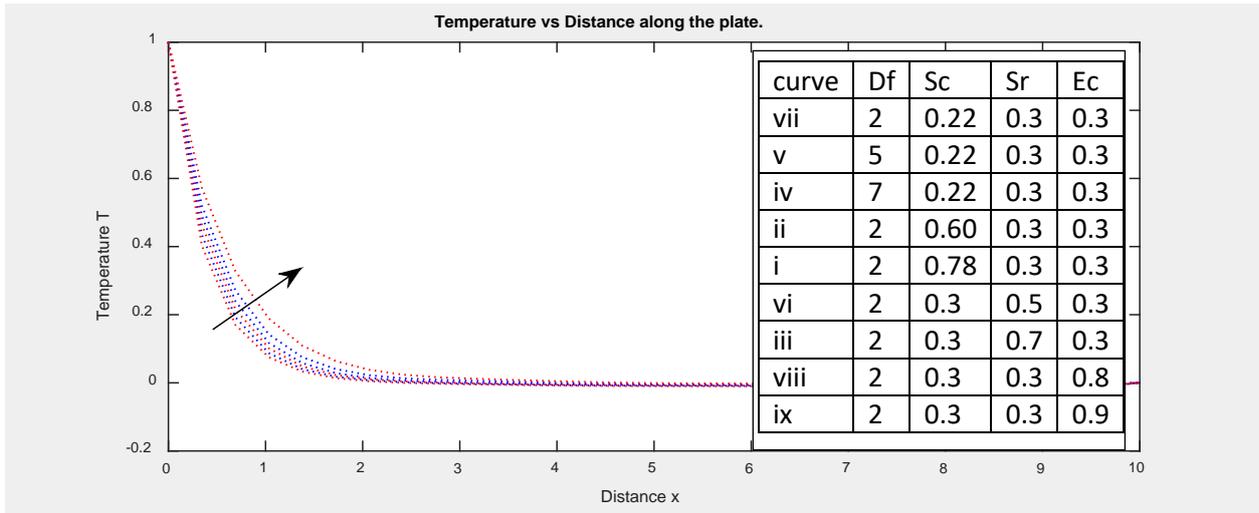


**Figure 10:** Primary velocity profiles for different values of Dufour number Df, Schmidt number Sc, Soret number Sr and Eckert number Ec for  $Gr_{\theta} = -0.5$ .

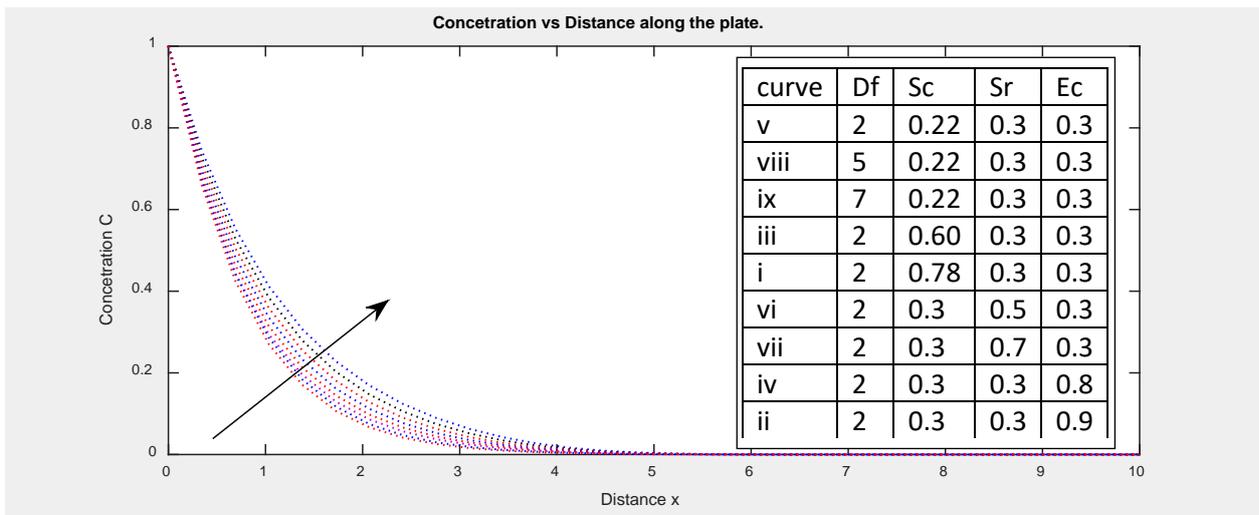


**Figure 11:** Secondary velocity profiles for different values of Dufour number Df, Schmidt number Sc, Soret number Sr and Eckert number Ec for  $Gr_{\theta} = -0.5$ .

From figure 13 it is noted that an increase in Df causes an increase in the concentration profiles. An increase in Schmidt number Sc causes decrease in the concentration profiles. Increase in Schmidt number lead to a decrease of molecular diffusivity, this lead to a decrease of concentration boundary layer. An increase in Sr causes an increase in the concentration profiles. Soret number (Sr) defines the effect of the temperature gradients inducing significant mass diffusion effects. Concentration profiles decrease with increase in the Eckert number.



**Figure 12:** Temperature profiles for different values of Dufour number Df, Schmidt number Sc, Soret number Sr and Eckert number Ec for  $Gr_{\theta} = -0.5$ .



**Figure 13:** Concentration profiles for different values of Dufour number Df, Schmidt number Sc, Soret number Sr and Eckert number Ec for  $Gr_{\theta} = -0.5$ .

### 5. Conclusion

An unsteady Magnetohydrodynamic fluid flow past contracting porous surface in a rotating system has been analysed.

The Reynolds number, radiation parameter, time, Eckert number and soret number tend to accelerate fluid flow in both primary, secondary velocity and temperature profiles; reverse effects is observed due to an increase in

rotation, permeability parameter, Dofour, Schmidt number. An increasing in rotation, permeability, radiation parameter, Dofour, solet number increases concentration while reverse effects is observed when Reynolds number, Schmidt number and Eckert number are increased.

The present work can provide basis for further research by considering turbulent flow over a contracting surface.

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